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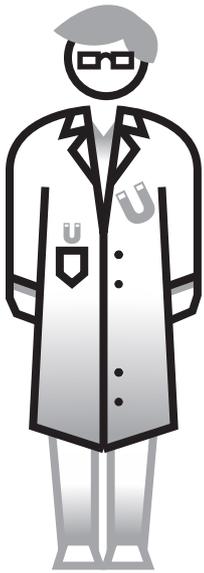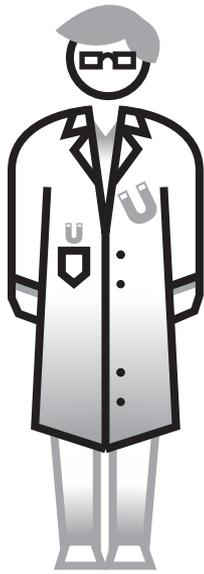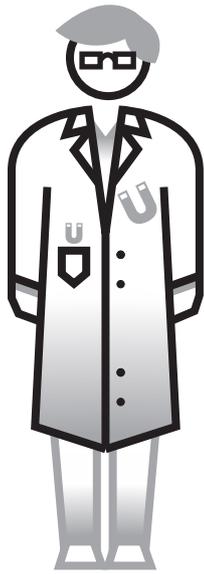
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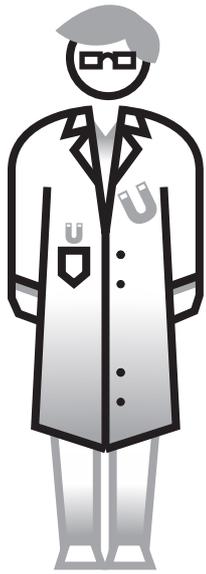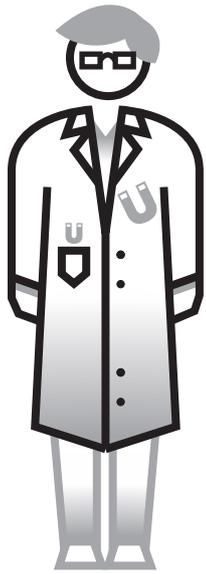
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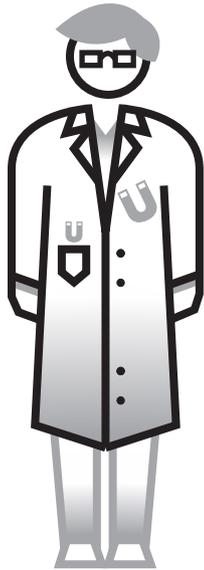
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FIG. 2. Magnetoresistance of a [(Fe 30 Å)/(Cr 9 Å)]$_{40}$ superlattice of 4.2 K. The current is along [110] and the field is in the layer plane along the current direction (curve a), in the layer plane perpendicular to the current (curve b), or perpendicular to the layer plane (curve c). The resistivity at zero field is 54 $\mu\Omega$ cm. There is a small difference between the curves in increasing and decreasing field (hysteresis) that we have not represented in the figure. The superlattice is covered by a 100-Å Ag protection layer. This means that the magnetoresistance of the superlattice alone should be slightly higher.

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The magnetoresistance of the Fe/Cr superlattices has been studied by a classical ac technique on small rectangular samples. Examples of magnetoresistance curves at 4.2 K are shown in Figs. 2 and 3. The resistance decreases during the magnetization process and becomes practically constant when the magnetization is saturated. The curves a and b in Fig. 2 are obtained for applied fields in the plane of layers in the longitudinal and transverse directions, respectively. The field H_S is the field needed to overcome the AF couplings and to saturate the magnetization (compare with Fig. 1). In contrast, fields applied perpendicularly to the layers (curve c) have to overcome not only the AF coupling but also the magnetic anisotropy, so that the magnetoresistance is saturated at a field higher than H_S.

The most remarkable result exhibited in Figs. 2 and 3 is the huge value of the magnetoresistance. For $t_{Cr} = 9$ Å and $T = 4.2$ K, see Fig. 2, there is almost a factor of 2 between the resistivities at zero field and in the saturated state, respectively (in absolute value, the resistivity change is about 23 $\mu\Omega$ cm). By comparison of the results for three different samples in Fig. 3, it can be seen


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R/R(H=0)

(Fe 30 Å / Cr 18 Å)$_{30}$

H_S

(Fe 30 Å / Cr 12 Å)$_{35}$

H_S

(Fe 30 Å / Cr 9 Å)$_{60}$

H_S

-40 -30 -20 -10 0 10 20 30 40

R

R/R(H=0)

1

(Fe 30 Å / Cr 18 Å)$_{30}$

H$_S$

0.

(Fe 30 Å / Cr 12 Å)$_{35}$

0.

H$_S$

0.

(Fe 30 Å / Cr 9 Å)$_{60}$

0.

H$_S$

0   -30   -20   -10   0   10   20   30   40   H

R

R / R (H = 0)

1

(Fe 30 Å / Cr 18 Å)$_{30}$

H$_S$

0.

(Fe 30 Å / Cr 12 Å)$_{35}$

0.

H$_S$

(Fe 30 Å / Cr 9 Å)$_{60}$

0.

H$_S$

0.

H

-30   -20   -10   0   10   20   30   40

R

R/R(H=0)

(Fe 30 Å / Cr 18 Å)$_{30}$

H_S

(Fe 30 Å / Cr 12 Å)$_{35}$

H_S

(Fe 30 Å / Cr 9 Å)$_{60}$

H_S

-30   -20   -10   0   10   20   30   40   H

H

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R

H

R/R(H=0)

(Fe 30 Å / Cr 18 Å)₃₀

H_S

(Fe 30 Å / Cr 12 Å)₃₅

H_S

(Fe 30 Å / Cr 9 Å)₆₀

H_S

0.8

0.7

0.6

0.5

-30   -20   -10   0   10   20   30   40

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H$_S$

0.8

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H$_S$

0.5

-30   -20   -10   0   10   20   30   40

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$(Fe\ 30\ \text{Å}\ /\ Cr\ 9\ \text{Å})_{60}$

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H_s

$(Fe\ 30\ \text{Å}\ /\ Cr\ 9\ \text{Å}\ )_{60}$

H_s

0.8

0.7

0.6

0.5

1

-30   -20   -10   0   10   20   30   40

R/R (H=0)

(Fe 30 Å / Cr 18 Å)₃₀

H_s

(Fe 30 Å / Cr 12 Å)₃₅

H_s

(Fe 30 Å / Cr 9 Å)₆₀

H_s

0.8

0.7

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-40 -30 -20 -10 0 10 20 30 40

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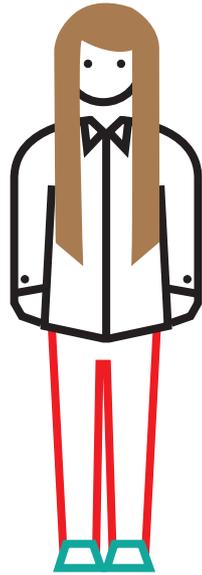
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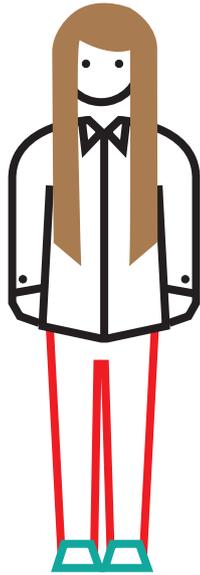
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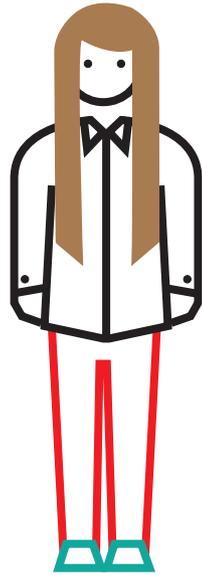
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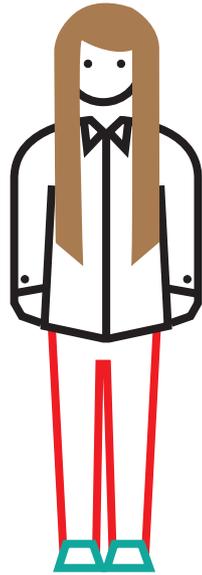
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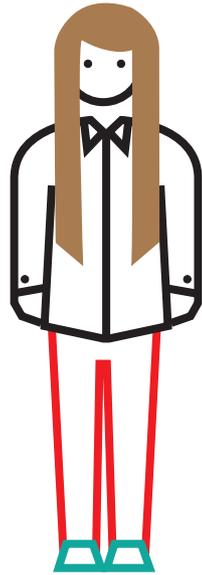
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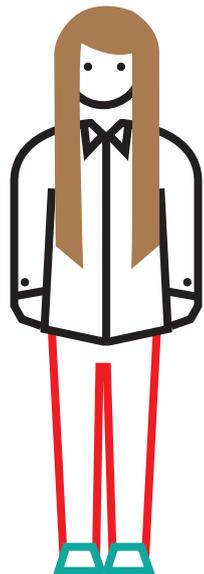
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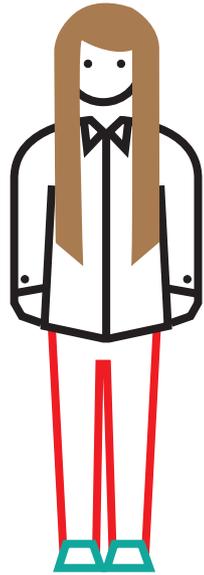
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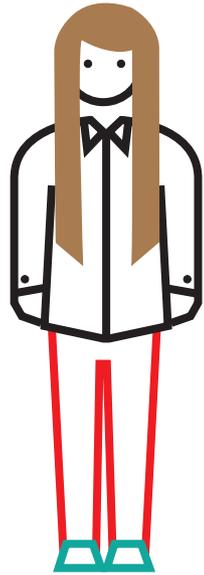
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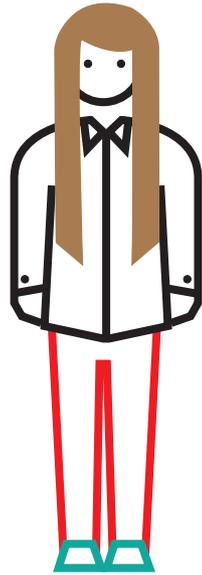
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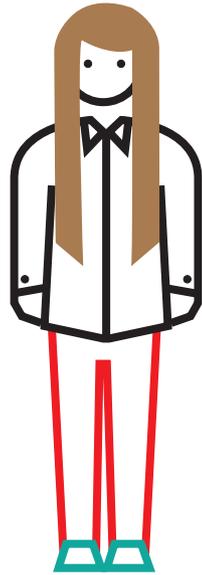
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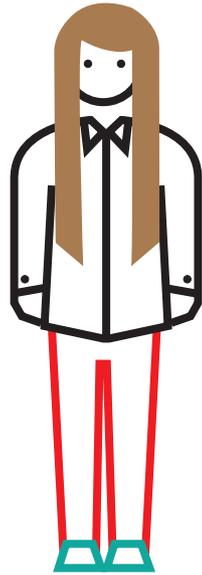
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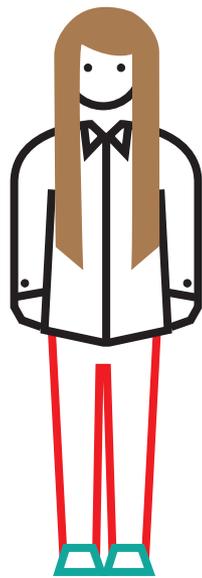
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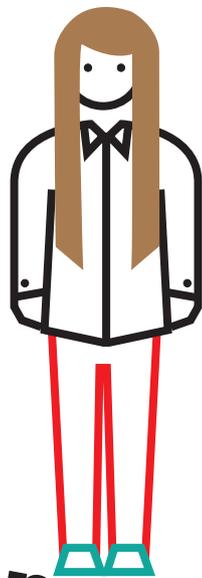
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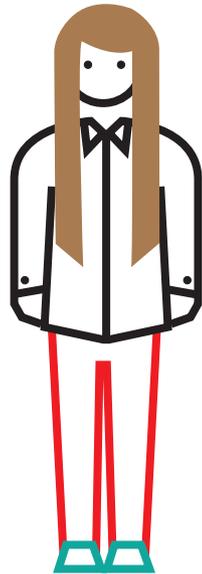
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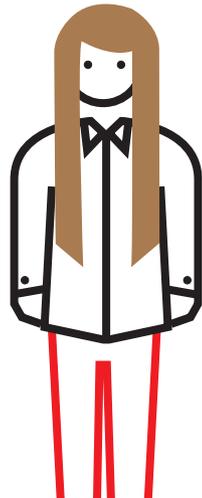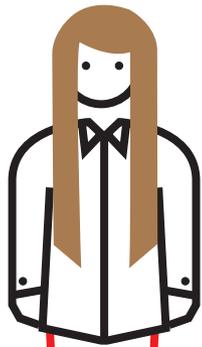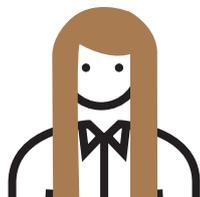
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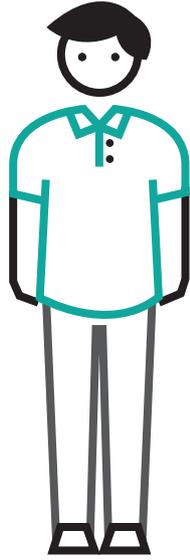
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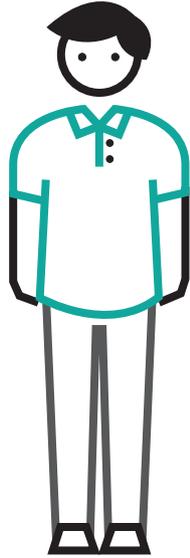
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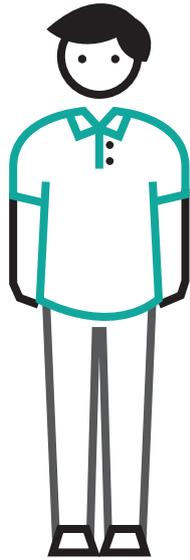
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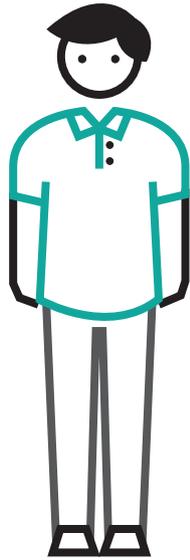
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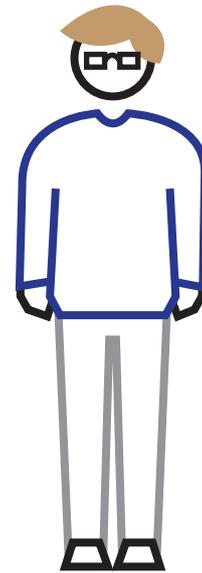
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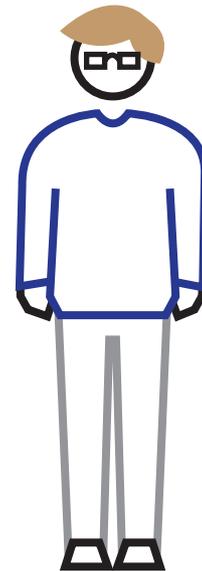
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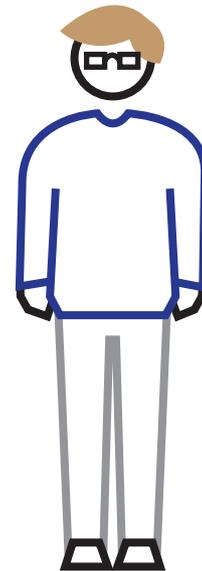
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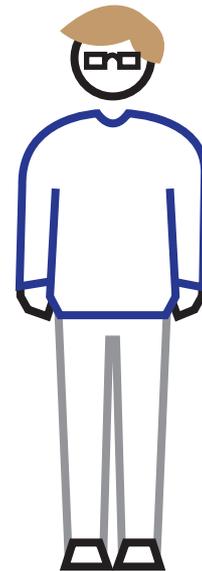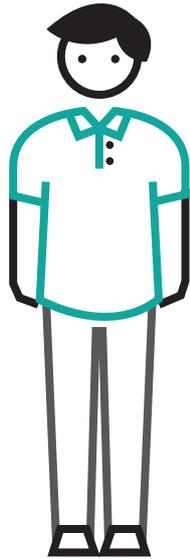
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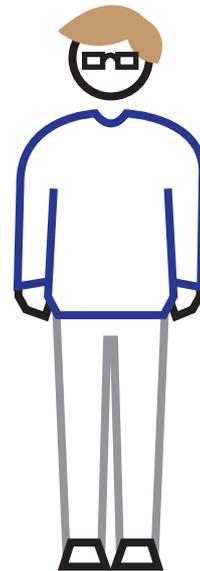
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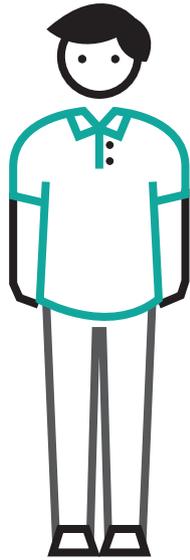
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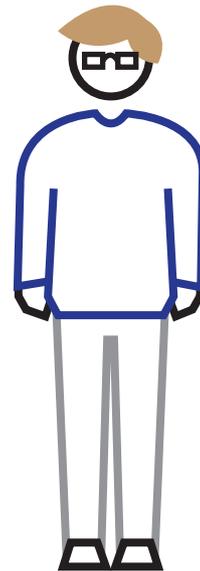
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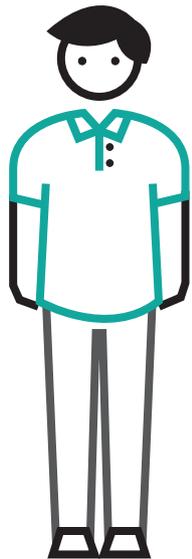
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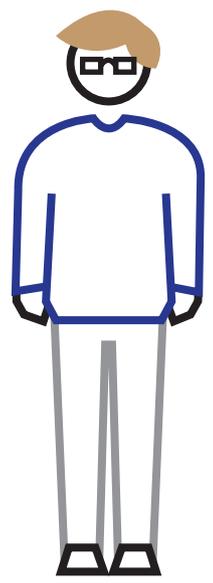
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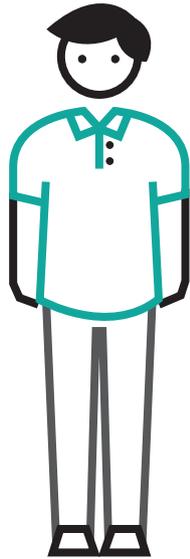
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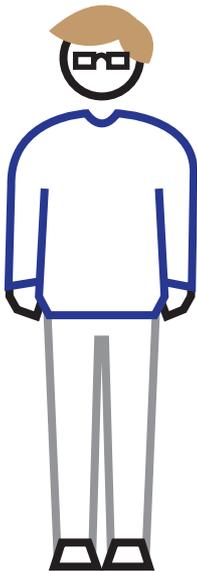
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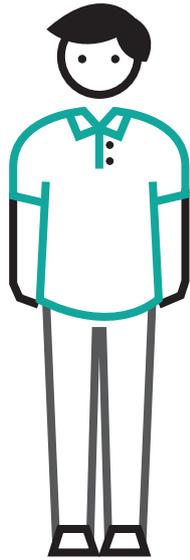
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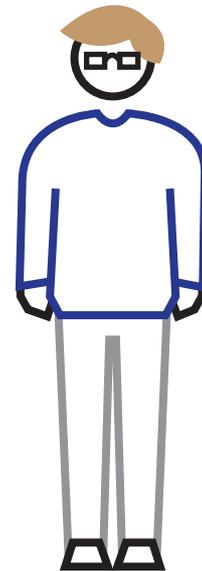
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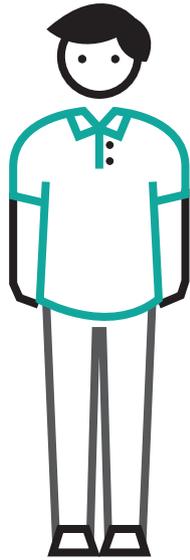
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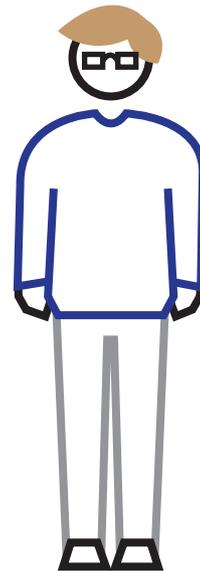
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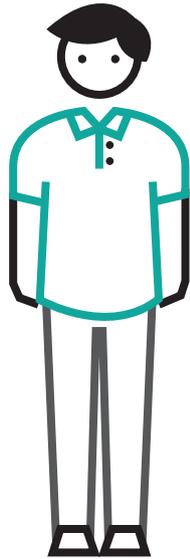
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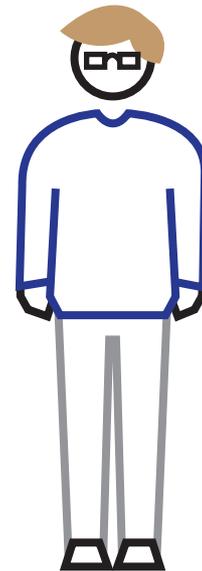
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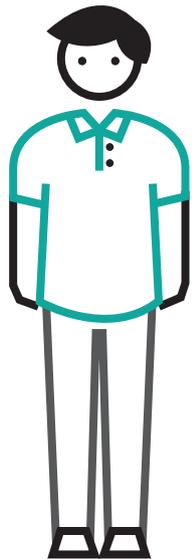
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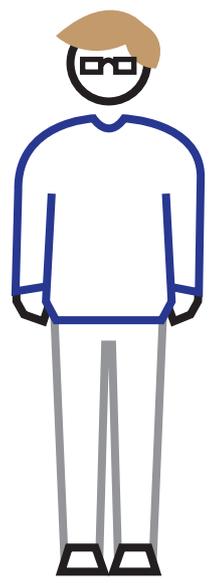
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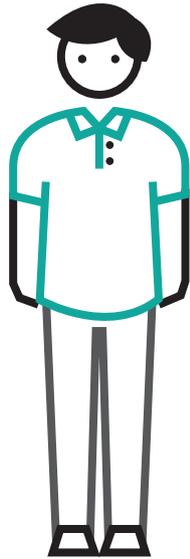
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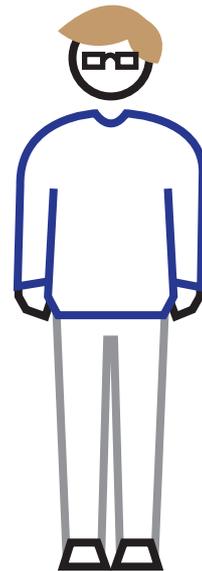
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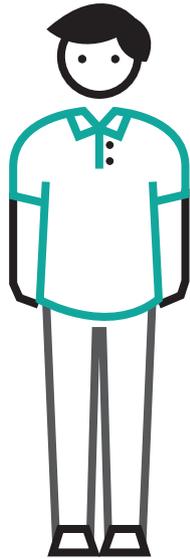
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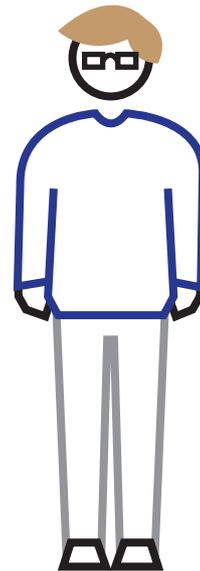
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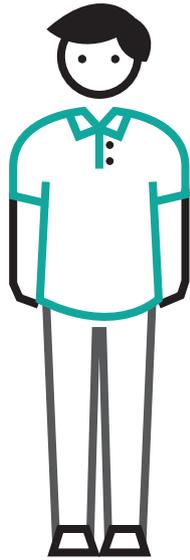
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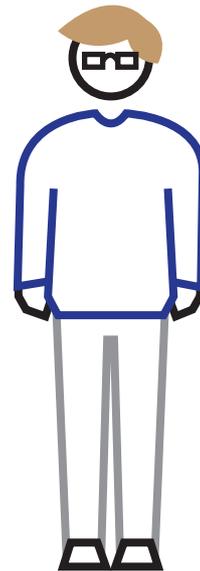
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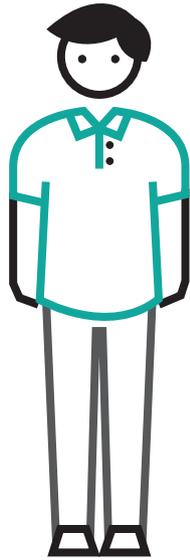
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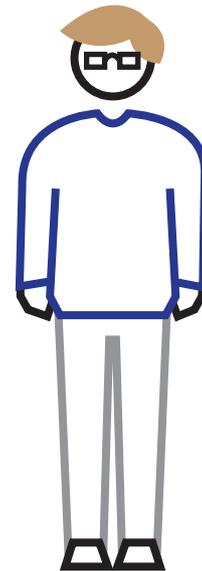
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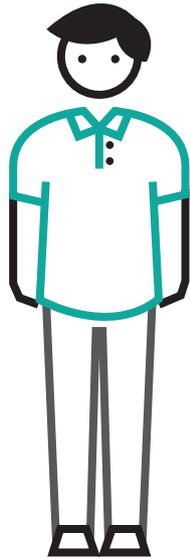
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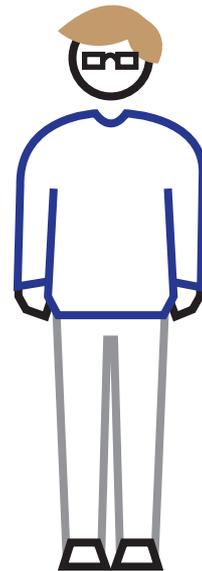
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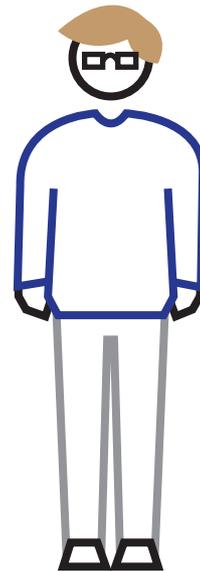
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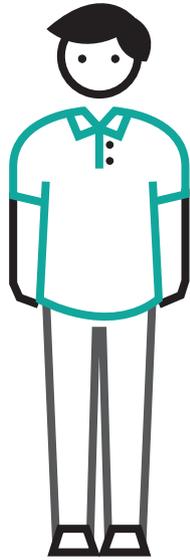
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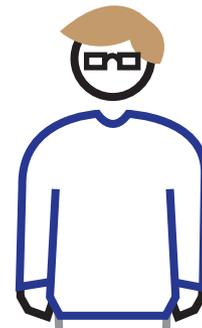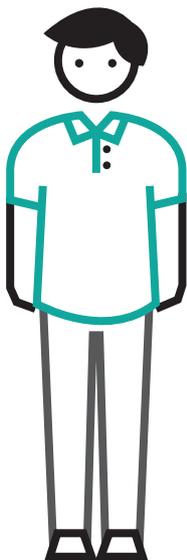
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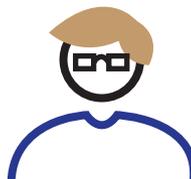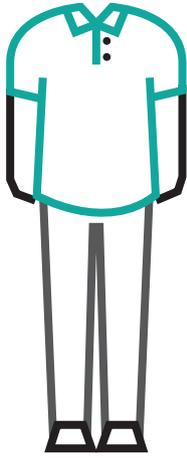
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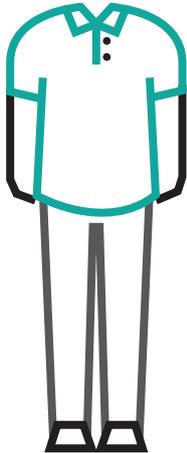
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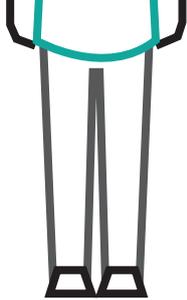
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